

## Heterogeneous Fenton degradation of Orange II by immobilization of Fe<sub>3</sub>O<sub>4</sub> nanoparticles onto Al-Fe pillared bentonite

Wenbing Li<sup>\*,\*\*,\*†</sup>, Dong Wan<sup>\*,†</sup>, Guanghua Wang<sup>\*,\*\*,\*</sup>, Kun Chen<sup>\*</sup>, Qin Hu<sup>\*</sup>, and Lulu Lu<sup>\*</sup>

<sup>\*</sup>College of Chemical Engineering and Technology, Wuhan University of Science and Technology, Wuhan 430081, China

<sup>\*\*</sup>Hubei Coal Conversion and New Carbon Materials Key Laboratory, Wuhan 430081, China

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**Abstract**—A novel catalyst, Fe<sub>3</sub>O<sub>4</sub> nanoparticle decorated Al-Fe pillared bentonite (Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B), was prepared by in situ precipitation oxidization method. The catalyst was characterized by SEM, XRD and Raman spectroscopy. The Fe<sub>3</sub>O<sub>4</sub> nanoparticles mainly exist on the surface or enter into the pore of bentonite, with better dispersing and less coaggregation. The catalytic activity of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B was investigated in the degradation of Orange II (OII) by heterogeneous Fenton-like process. The effects of initial concentration of hydrogen peroxide, catalyst loading, temperature and initial pH on the degradation of OII were investigated. The Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B showed higher degradation efficiency of OII than bare Fe<sub>3</sub>O<sub>4</sub> or Al-Fe-P-B in the degradation experiment. The enhanced catalytic activity of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B in heterogeneous Fenton system was due to the synergistic effect between Al-Fe-P-B and Fe<sub>3</sub>O<sub>4</sub>. The novel catalyst can achieve solid-liquid separation easily by sample magnetic separation and has a good reusability and stability.

Keywords: Magnetic Bentonite, Heterogeneous Catalyst, Degradation, Orange II, Magnetic Separation

### INTRODUCTION

Fenton and Fenton-like technology have been extensively studied as one of the best options for the degradation of various recalcitrant organic pollutants in water. However, there is a non-ignorable drawback of traditional homogeneous Fenton that it is difficult to remove the iron sludge after the treatment and may cause secondary pollution [1,2]. Recently, heterogeneous Fenton-like systems using solid catalysts have been developed. Most of the researches on heterogeneous Fenton-like catalysts have been focused on iron supported materials, such as zero valent iron (Fe<sup>0</sup>) [3], iron-based clays [4] and iron oxide minerals [5]. Among these catalysts, iron oxide minerals, especially magnetite (Fe<sub>3</sub>O<sub>4</sub>) nanoparticles, attracted more attention, since Fe<sub>3</sub>O<sub>4</sub> contains both Fe<sup>2+</sup> and Fe<sup>3+</sup>, which are the crucial cations for initiation of Fenton reaction according to the classical Haber-Weiss mechanism [6]. Moreover, with an inverse spinel crystal structure, the electrons can transfer between Fe<sup>2+</sup> and Fe<sup>3+</sup> in the octahedral sites, allowing the Fe species to be reversibly oxidized and reduced while keeping the same structure [7]. In addition, Fe<sub>3</sub>O<sub>4</sub> nanoparticles are magnetic and can be easily separated from the terminal solution by magnetic separation.

With the advantages of strong catalytic activity, long-term stability, excellent environment-friendly and, especially, the intrinsic peroxidase-like activity [6], Fe<sub>3</sub>O<sub>4</sub> nanoparticles are investigated as ideal heterogeneous Fenton-like catalysts for the removal of environmental contaminants, including phenol [7], aniline [8], 2,4-dichlorophenol [9], p-nitrophenol [10] and dye pollutants [11]. However, the coaggregation of Fe<sub>3</sub>O<sub>4</sub> nanoparticles often constitutes a chal-

lenge that nanomaterials have to be confronted, since the coaggregation decreases the effective surface active sites of nanoparticles and thus reduces their catalytic activities, especially in water solution [12]. Several methods have been accordingly developed for overcoming the coaggregation of nanoparticles. Recently, immobilized Fe<sub>3</sub>O<sub>4</sub> nanoparticles on solid supports during the preparation process were found to be effective to prevent coaggregation and improve the catalytic activity. The supports can be organic and inorganic materials, such as activated carbon [13], multiwalled carbon nanotubes [14], mesocellular carbon foam [15] and poly(3,4-ethylenedioxythiophene) [16]. It is well accepted that the supporting materials must be of high stability, low cost and environmental harmony.

Bentonite is a kind of natural 2:1 type layered clay mineral with high stability, microporosity, larger surface area and low cost that has been widely used in a number of industrial branches [17]. After intercalating by polymeric inorganic oxocations, the stability, surface area and catalytic performance of bentonite could be promoted effectively [18]. Many researches on intercalated bentonite have been focused on Al-Fe pillared bentonite, which could be used as a heterogeneous Fenton-like catalyst [19-21]. With so many excellent properties, pillared bentonite may be particularly suitable as a support for the synthesis of magnetic nanoparticles. Thus, immobilizing Fe<sub>3</sub>O<sub>4</sub> nanoparticles on Al-Fe pillared bentonite may have some advantages. On one hand, the coaggregation of Fe<sub>3</sub>O<sub>4</sub> nanoparticles could be prevented effectively. On the other hand, the Al-Fe pillared bentonite may achieve solid-liquid separation easily by magnetic separation technology. The most important is that there may be a synergistic effect between the Al-Fe pillared bentonite and Fe<sub>3</sub>O<sub>4</sub> nanoparticles, which can improve the catalytic activity of the catalyst. However, so far, few attempts to synthesize pillared bentonite-supported Fe<sub>3</sub>O<sub>4</sub> composite could be found in literatures, and the magnetic bentonite was mainly prepared to act as adsorbent instead

<sup>†</sup>To whom correspondence should be addressed.

E-mail: wandongchn@126.com, liwenbing@126.com

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of heterogeneous Fenton-like catalyst [22-26]. Since the mimic enzyme catalysis process is becoming a novel challenging field and a hot area of research in the green chemical engineering, it is urgent to develop a low cost, environment-friendly and high-efficiency heterogeneous catalyst to meet the needs of environmental protection.

In our previous research, we used Al-pillared bentonite to immobilize  $\text{Fe}_3\text{O}_4$  nanoparticles by in situ co-precipitation method (c- $\text{Fe}_3\text{O}_4$ ) [27]. The average size of  $\text{Fe}_3\text{O}_4$  nanoparticles was around 20-25 nm. However, in this post-study survey, we found that  $\text{Fe}_3\text{O}_4$  nanoparticles with diameter ranging from 40 to 100 nm, synthesized through precipitation oxidization method (o- $\text{Fe}_3\text{O}_4$ ), had higher catalytic performance and stability, which can be seen from Fig. S1 and Fig. S2 in supplementary data. From the XRD patterns of these two kinds of  $\text{Fe}_3\text{O}_4$  nanoparticles (Fig. S3), we can find that the o- $\text{Fe}_3\text{O}_4$  has higher crystallinity than c- $\text{Fe}_3\text{O}_4$ . It is the higher crystallinity and  $\text{Fe}^{II}/\text{Fe}^{III}$  ratio that give o- $\text{Fe}_3\text{O}_4$  better oxidation efficiency for dye removal. Similar results were also found by Xue et al. [28]. On the other hand, Al-Fe pillared bentonite showed higher adsorption and catalytic performance than Al pillared bentonite [21]. Thus, we propose a new strategy toward Al-Fe pillared bentonite-supported  $\text{Fe}_3\text{O}_4$  nanoparticles ( $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ ). The nanocomposites were prepared through in situ precipitation oxidization method for the first time and further used for the removal of organic pollutants in water. As known, Orange II(OII) is a typical azo dye and has been selected as a model dyeing pollutant in many investigations because of its widespread application and recalcitrant nature [4,21,29]. To evaluate the feasibility of the prepared nanocomposites to be used as heterogeneous Fenton-like catalyst in the organic wastewater treatment, Orange II was selected as the target pollutant. The reaction conditions of Orange II in the Fenton processes in the presence of nanocomposites were optimized. The microstructure, morphology and stability of the nanocomposites were also investigated.

## MATERIALS AND METHODS

### 1. Materials

Natural bentonite was procured from Shanghai No. 4 Reagent & H.V. Chemical Co., Ltd., China. Orange II(OII) was obtained from Shanghai Zhanyun Chemical Co., Ltd., China. All chemicals were of analytical grade and used as received. In the experiments, distilled water was used for preparing the solutions and suspensions.

### 2. Preparation of $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ Catalyst

The Al-Fe pillared bentonite (Al-Fe-P-B) was prepared by pillaring the bentonite through cation-exchange process as described in the literature [21]. The nanocomposites were synthesized by in situ precipitation oxidization method. 2 g Al-Fe-P-B was added into a 500 mL flask containing 200 mL distilled water with constantly stirring. The solution was bubbled with  $\text{N}_2$  flow for 15 min to remove the dissolved oxygen and placed in a 95 °C water bath, and then 8 g  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$  and 3.6 g  $\text{NaNO}_3$  were added into the flask. Afterwards, 40 mL ammonia was added dropwise ( $2 \text{ mL min}^{-1}$ ) into the heating solution while keeping vigorous stirring and stable  $\text{N}_2$  flow during the entire reaction period. After that, the solution was heated at 95 °C for another hour, and then cooled to room tem-

perature. The precipitate was isolated by a permanent magnet. After repeated washing with deionized water and absolute ethanol under ultrasonication, the formed  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  nanocomposites were dried in a vacuum oven at 100 °C for 12 h.  $\text{Fe}_3\text{O}_4$  was synthesized as above procedure without adding Al-Fe-P-B. All the products were stored in a desiccator under ambient temperature for further experiments.

### 3. Characterization

X-ray diffraction (XRD) patterns of the samples were recorded by a Rigaku D/max-RB diffractometer (Rigaku, Japan) at 40 kV and 30 mA using filtered Cu  $K\alpha$  radiation ( $\lambda=0.15418 \text{ nm}$ ). Raman spectra were obtained using the DXR laser micro-Raman spectrometer (Thermo Scientific, America) at a laser wavelength of 780 nm. Micrographs of the samples were taken using a Nova400 Nano SEM (FEI, America). Before observation of SEM, all samples were fixed on silicon wafer and coated with gold.

### 4. Degradation of Orange II by Heterogeneous Fenton Experiments

The experiments were carried out in a conical flask with a stopper (containing 200 mL of reaction solution). The dosage of catalyst was 0-2.0  $\text{g L}^{-1}$  while the concentrations of OII and  $\text{H}_2\text{O}_2$  were 0.23  $\text{mmol L}^{-1}$  and 0-25  $\text{mmol L}^{-1}$ , respectively. All experiments were carried out under constant stirring to make good catalyst dispersion. The initial pH of solution was adjusted by  $\text{H}_2\text{SO}_4$  and NaOH. Before reaction, the suspension containing catalyst and OII was stirred for 60 min to achieve adsorption equilibrium. A 1-mL sample was withdrawn from the reactor to analyze the decolorization efficiency of 0 min. The Fenton reaction was initiated when  $\text{H}_2\text{O}_2$  was added to the OII solution. After the oxidation reaction, the catalyst was repeated washing and dried for reusing.

### 5. Analyses

At given intervals of degradation, a sample was analyzed by UV-Vis spectroscopy (Ultrospec 3300 pro, GE Healthcare Bio-Sciences China Ltd.) at a wavelength of 484 nm, which is the maximum absorption wavelength of Orange II [4]. The concentration of Orange II was converted through the standard curve method of dyes. The concentration of  $\text{Fe}^{2+}$  and total iron concentration ( $\Sigma\text{Fe}^{III}$ ) in the solution was measured by the 1,10-phenantroline spectrophotometric method [29]. The chemical oxygen demand ( $\text{COD}_C$ ) was determined by dichromate method. To eliminate the interference of  $\text{H}_2\text{O}_2$  with  $\text{COD}_C$  measurements, the reaction was finally blocked by raising the pH to 9-10, adding  $\text{MnO}_2$  and allowing the samples to sit overnight [30].

## RESULTS AND DISCUSSION

### 1. Characterization of Catalyst

The morphologies of pillared bentonite and catalysts were characterized by SEM. The SEM images in Fig. 1(a) show that the pillared bentonite is layer structure and has a coarse porous surface. The synthesized  $\text{Fe}_3\text{O}_4$  (Fig. 1(b)) are spherical-like mostly and dramatically co-aggregated together, while in the sample of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  (Fig. 1(c)), the supported  $\text{Fe}_3\text{O}_4$  nanoparticles exist on the surface or enter into the pore of bentonite, with better dispersing and less co-aggregation. Besides, the  $\text{N}_2$  adsorption-desorption isotherms for  $\text{Fe}_3\text{O}_4$  and  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  were also recorded, which

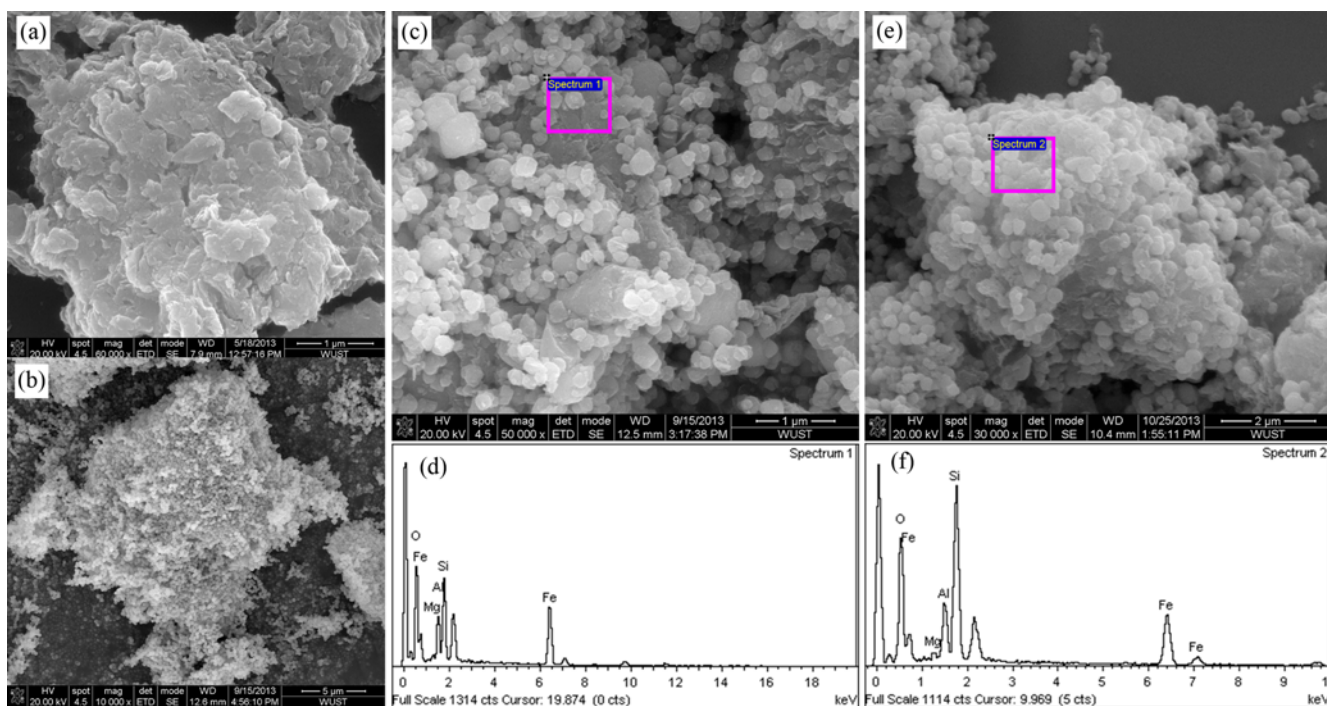


Fig. 1. SEM photograph of Al-Fe-P-B (a), Fe<sub>3</sub>O<sub>4</sub> (b), Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B (c) and reused Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B (e) and EDS spectra of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B (d) and reused Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B (f).

is shown in Fig. S4 in supplementary data. The specific surface areas calculated by using a BET equation are found to be 4.68 and 53.02 m<sup>2</sup> g<sup>-1</sup> for Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B, respectively. And wide hysteresis area of N<sub>2</sub> adsorption/desorption isotherms can be clearly seen in the case of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B, suggesting the wide distributions of pores in the nanocomposites. Although the products have experienced repeated washing in water and methanol under ultrasonication before SEM measurements, almost all magnetite nanoparticles are still found on the bentonite surface. This indicates the strong interaction between Al-Fe-P-B and magnetite nanoparticles. The diameter of Fe<sub>3</sub>O<sub>4</sub> nanoparticles ranges from 40 to 100 nm. The EDS spectra of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B are shown in Fig. 1(d). It can be found that the nanocomposite mainly consists of O, Si, Al, Mg and Fe. The image of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B nanoparticles reused for three times in Fig. 1(e) shows no obvious change of structure of the catalyst after oxidation reaction. The saturation magnetization of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B is 30.9 emu g<sup>-1</sup>, which can be seen in Fig. S5 in supplementary data. Such a high magnetization makes the nanocomposite be quickly separated from its dispersion with a magnet.

The X-ray diffraction patterns of the samples are shown in Fig. 2(a). Diffraction peaks assigned to bentonite at  $2\theta=5.5^\circ$  [17,18] can be seen for Al-Fe-P-B and Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B nanocomposites, indicating that the bentonite structure is not destroyed after treatment by pillaring process and the chemical precipitation of Fe<sub>3</sub>O<sub>4</sub>. As shown in Fig. 2(a), eight characteristic peaks for Fe<sub>3</sub>O<sub>4</sub> ( $2\theta=18, 30, 35.5, 37, 43, 53.4, 57$  and  $62.5$ ) are observed for the synthesized Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B nanocomposites. And no other peaks corresponding to the hematite are detected in the XRD patterns, indicating that the Fe<sub>3</sub>O<sub>4</sub> nanoparticles in the composites are pure Fe<sub>3</sub>O<sub>4</sub> with inverse spinel structure [31].

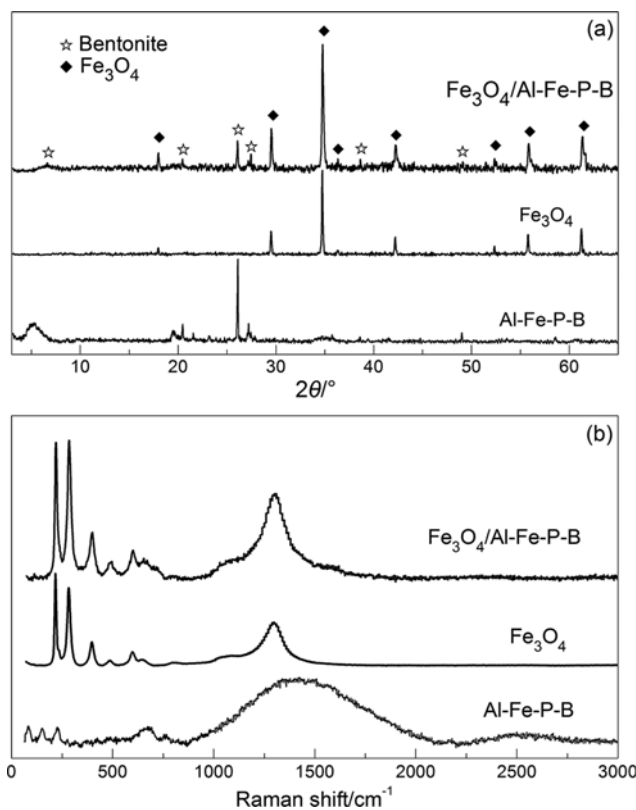


Fig. 2. XRD patterns (a) and Raman spectra (b) of the samples.

Fig. 2(b) shows the Raman spectra of the samples. The peak found at 152 cm<sup>-1</sup> is attributed to the O-Al-O symmetric bending

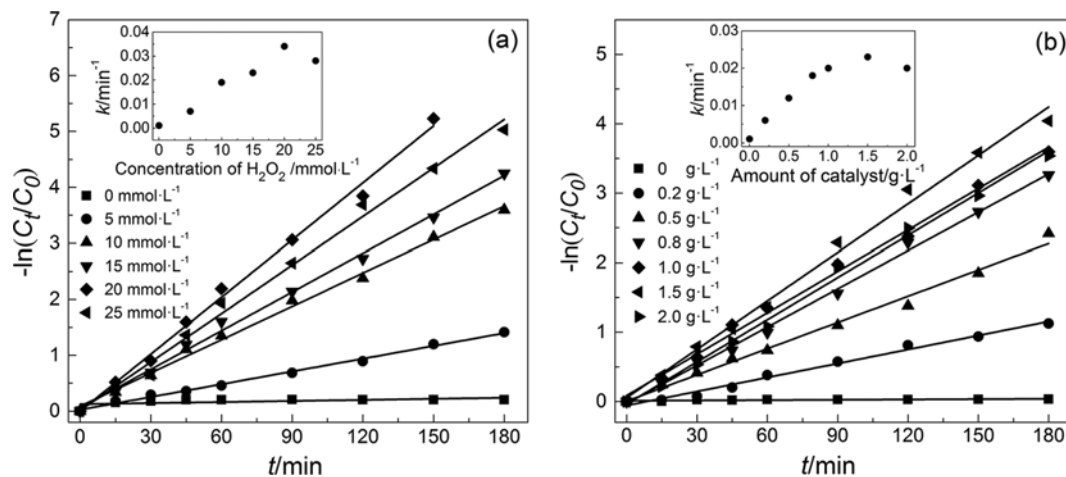


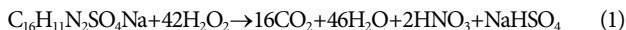
Fig. 3. The effects of  $\text{H}_2\text{O}_2$  concentration (a) and amount of catalyst (b) on the degradation efficiency of Orange II. Inset: correlation of the apparent pseudo-first-order rate constant ( $C_{\text{OII}}=0.23 \text{ mmol}\cdot\text{L}^{-1}$ ,  $1.0 \text{ g}\cdot\text{L}^{-1}$  of catalyst,  $10 \text{ mmol}\cdot\text{L}^{-1}$  of  $\text{H}_2\text{O}_2$ ,  $\text{pH}=3.5$ ,  $40^\circ\text{C}$ ).

mode of the  $\text{AlO}_6$  octahedron. The band at  $704 \text{ cm}^{-1}$  can be assigned to the symmetric stretching of the Si-O-Si group in the  $\text{SiO}_4$  tetrahedral layer of the phyllosilicates [32]. The bands at 232, 299, 410, 501 and  $615 \text{ cm}^{-1}$  are characteristic peaks of  $\text{Fe}_3\text{O}_4$  [33], which are also found in the Raman spectra of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ . It is in conformity with the XRD analysis.

## 2. Catalytic Performance of Catalysts

### 2-1. Effect of the Hydrogen Peroxide Concentration

The effect of hydrogen peroxide was analyzed by varying its initial concentration between  $0 \text{ mmol L}^{-1}$  and  $25 \text{ mmol L}^{-1}$  (Fig. 3(a)). Under all tested conditions, the OII degradation was observed to approximately follow a pseudo-first-order reaction in kinetics, which can be expressed as  $-\ln(C_t/C_0)=kt$ , where  $C_0$  and  $C_t$  ( $\text{mg}\cdot\text{L}^{-1}$ ) is the concentration of OII at 0 min and  $t$  min,  $k$  ( $\text{min}^{-1}$ ) is the apparent pseudo-first-order rate constant and  $t$  (min) is the reaction time. The  $k$  constants were obtained from the slopes of the straight lines by plotting  $-\ln(C_t/C_0)$  as a function of time  $t$ , through regression [34]. Good correlation coefficients ( $R^2>0.98$ ) are obtained in our systems. From Fig. 3(a) there is little OII removed in the absence of  $\text{H}_2\text{O}_2$ . According to the previous study, 42 mol of  $\text{H}_2\text{O}_2$  was theoretically needed for complete degradation of 1 mol of the dye:



Based on this equation, the necessary amount of  $\text{H}_2\text{O}_2$  in the present study for complete degradation of  $100 \text{ mg L}^{-1}$  ( $0.23 \text{ mmol L}^{-1}$ ) of OII is  $9.54 \text{ mmol L}^{-1}$ . It is observed that the degradation rate of OII increases observably when  $\text{H}_2\text{O}_2$  concentration increases from 0 to  $10 \text{ mmol L}^{-1}$ . Since the OII degradation is directly related to the concentration of the  $\bullet\text{OH}$  produced by the catalytic decomposition of  $\text{H}_2\text{O}_2$ , more OII decomposition is expected with a higher  $\text{H}_2\text{O}_2$  concentration. However, a significant improvement is not seen when the  $\text{H}_2\text{O}_2$  concentration increased to  $15 \text{ mmol L}^{-1}$ , which can be explained by the scavenging effect of  $\bullet\text{OH}$  by  $\text{H}_2\text{O}_2$ :



The oxidation potential of  $\bullet\text{OOH}$  is much smaller than that of the  $\bullet\text{OH}$  species. Therefore, it makes the reaction slow down though

the rate constant still increases. However, when the  $\text{H}_2\text{O}_2$  concentration increases to  $20 \text{ mmol L}^{-1}$ , the degradation process turns to significantly accelerate. The main reason for this phenomenon may be that the increase of  $\text{H}_2\text{O}_2$  dosage increases the dissolved iron concentration under acid condition and induces the homogeneous catalytic oxidation. The rate constant is reduced slightly at a much higher  $\text{H}_2\text{O}_2$  concentration ( $25 \text{ mmol L}^{-1}$ ), due to the accelerating of the Eq. (2).

### 2-2. Effect of Catalyst Dosage

As expected, OII degradation rate increases dramatically as the amount of employed catalyst increases from 0 to  $1.0 \text{ g L}^{-1}$  (Fig. 3(b)), due to the increasing amount of active sites for the formation of  $\bullet\text{OH}$  and, maybe equally important, for OII adsorption. Nevertheless, when catalyst addition is further increased to  $2.0 \text{ g L}^{-1}$ , the degradation of OII does not enhance but slightly decreases, because of the agglomeration of nanoparticles and the scavenging of hydroxyl radicals or other radicals by present iron species through undesirable reactions (3)-(5) [9].



### 2-3. Effect of Temperature

The degradation efficiency of OII increases with the increase of temperature, as seen from Fig. 4. According to previous study [4], the change in enthalpy that follows the oxidative degradation of OII is positive while the process is endothermic. Accordingly, the increase of the reaction temperature is beneficial for the degradation of OII solutions. In addition, the  $k$  constant at different temperatures can be expressed by the Arrhenius equation as follows:

$$k=A\times\exp(-E_a/RT) \quad (6)$$

where  $k$  is the rate constant,  $A$  is a pre-exponential factor,  $E_a$  is reaction activation energy ( $\text{kJ mol}^{-1}$ ),  $R$  is the gas constant ( $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ ), and  $T$  is the absolute temperature (K). According to the equation, we have

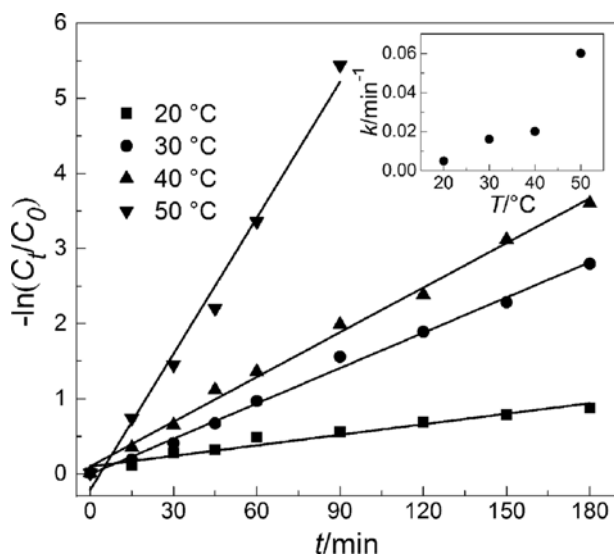


Fig. 4. The effect of temperature on the degradation efficiency of Orange II. Inset: correlation of the apparent pseudo-first-order rate constant with temperature ( $C_{OII}=0.23 \text{ mmol}\cdot\text{L}^{-1}$ ,  $10 \text{ mmol}\cdot\text{L}^{-1}$  of  $\text{H}_2\text{O}_2$ ,  $1.0 \text{ g}\cdot\text{L}^{-1}$  of catalyst,  $\text{pH}=3.5$ ).

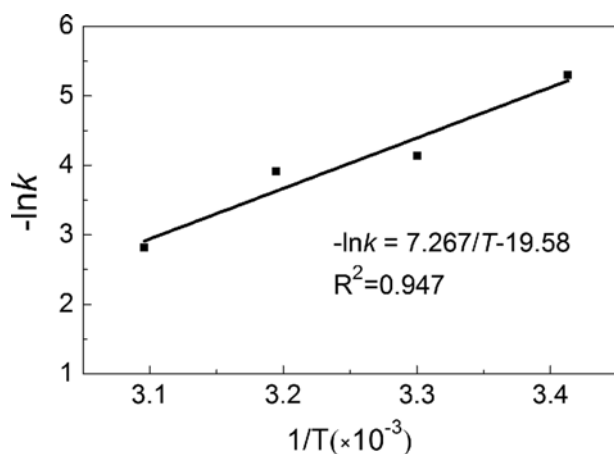


Fig. 5. Arrhenius plots for degradation of Orange II catalyzed by magnetic bentonite.

$$-\ln k = E_a/RT - \ln A \quad (7)$$

In terms of the data in Fig. 4, by plotting  $\ln k$  versus  $1/T$ , we obtained the  $E_a$  value from the slope of the straight line (Fig. 5). The  $E_a$  value calculated is  $60.42 \text{ kJ mol}^{-1}$ , which is similar to the result reported earlier [34].

#### 2-4. Effect of Initial pH

The effect of initial solution pH on the degradation rate of OII is shown in Fig. 6. When the initial pH is 3.0, OII can be quickly degraded in 120 min under the adopted conditions. But as the initial pH rises, the degradation becomes much slower. The increased degradation efficiency at lower pH values can be attributed to the higher oxidation potential of hydroxyl radicals, whose generation rate is enhanced in a lower pH value [14]. The previous studies approved that lower pH could increase the electrostatic attraction

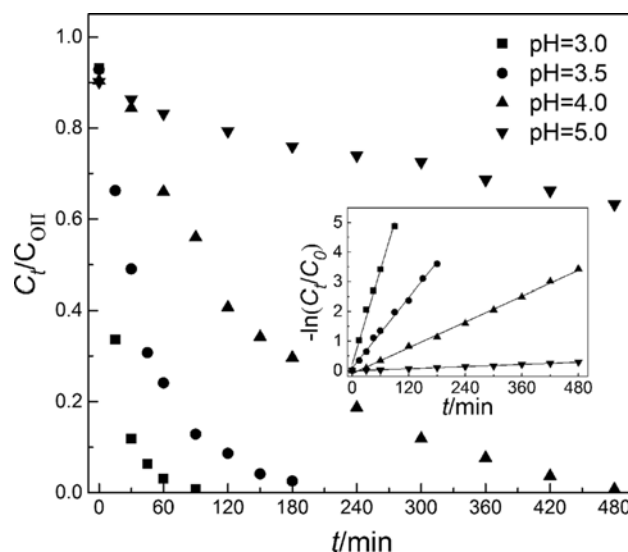


Fig. 6. The effect of initial pH on the degradation efficiency of Orange II. Inset: fitted by pseudo-first-order rate law ( $C_{OII}=0.23 \text{ mmol}\cdot\text{L}^{-1}$ ,  $10 \text{ mmol}\cdot\text{L}^{-1}$  of  $\text{H}_2\text{O}_2$ ,  $1.0 \text{ g}\cdot\text{L}^{-1}$  of catalyst,  $40^\circ\text{C}$ ).

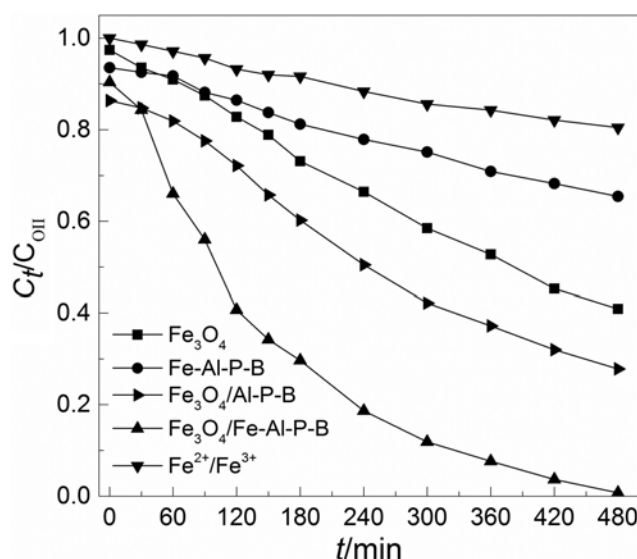


Fig. 7. Degradation of Orange II using different catalysts ( $C_{OII}=0.23 \text{ mmol}\cdot\text{L}^{-1}$ ,  $10 \text{ mmol}\cdot\text{L}^{-1}$  of  $\text{H}_2\text{O}_2$ ,  $0.5 \text{ g}\cdot\text{L}^{-1}$  of  $\text{Fe}_3\text{O}_4$  or Al-Fe-P-B,  $1.0 \text{ g}\cdot\text{L}^{-1}$  of  $\text{Fe}_3\text{O}_4$ /Al-Fe-P-B,  $\text{pH}=4$ ,  $40^\circ\text{C}$ ).

between dye molecules and surfaces of magnetite, promoting the formation of metal oxide-pollutant inner-sphere complexes, which has an advantage to the degradation of pollutants [9,34]. Moreover, in Fig. 6 all the degradation processes also comply with pseudo-first-order rate law.

#### 2-5. The Synergistic Effect between Fe<sub>3</sub>O<sub>4</sub> and Al-Fe-P-B

To compare with the past system [27], the removal rates of OII by  $\text{Fe}_3\text{O}_4$ /Al-P-B and  $\text{Fe}_3\text{O}_4$ /Al-Fe-P-B in the same reaction condition are shown in Fig. 7. Before the addition of  $\text{H}_2\text{O}_2$ , the removal of OII only relies on adsorption. It can be seen that the removal rates of  $\text{Fe}_3\text{O}_4$ /Al-P-B and  $\text{Fe}_3\text{O}_4$ /Al-Fe-P-B just by adsorption are 14.1% and 9.6%, respectively. Since the specific surface area of

$\text{Fe}_3\text{O}_4/\text{Al-P-B}$  ( $103.83 \text{ m}^2 \text{ g}^{-1}$ ) in previous study is higher than that of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  ( $53.02 \text{ m}^2 \text{ g}^{-1}$ ), and the average size of  $\text{Fe}_3\text{O}_4$  nanoparticles is much smaller in  $\text{Fe}_3\text{O}_4/\text{Al-P-B}$ , the  $\text{Fe}_3\text{O}_4/\text{Al-P-B}$  can be able to adsorb more OII molecules. However, after the addition of  $\text{H}_2\text{O}_2$ , it can be obviously found that the degradation efficiency of OII in the present of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  is much higher than that of  $\text{Fe}_3\text{O}_4/\text{Al-P-B}$  through heterogeneous Fenton reaction. The enhanced catalytic activity of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  may due to the higher stability of  $\text{Fe}_3\text{O}_4$  nanoparticles which synthesized through precipitation oxidization method (Fig. S1-S3 in supplementary data). Moreover, in our previous study [21], we concluded that the immobilized Fe-ions in Al-Fe-P-B were beneficial for the accessibility of the catalyst to reactants (OII and  $\text{H}_2\text{O}_2$ ). Thus, the Al-Fe-P-B can provide more available and effective contact surface areas between reactants and active sites than Al-P-B. The adsorbed OII molecules in the immediate vicinity of immobilized Fe-ions are easily attacked by the generated  $\bullet\text{OH}$ . Therefore, it is more efficient to use Al-Fe-P-B as supporter. As a result, the catalytic efficiency has improved dramatically in the new system.

To investigate the synergistic effect between  $\text{Fe}_3\text{O}_4$  and Al-Fe-P-B, a comparison of removal rates of OII by  $\text{Fe}_3\text{O}_4$ , Al-Fe-P-B and  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  is also shown in Fig. 7. Since the ratio of  $\text{Fe}_3\text{O}_4$  in  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  was 50%, the dosages of three catalysts in this experiment were  $0.5 \text{ g L}^{-1}$  for  $\text{Fe}_3\text{O}_4$  and Al-Fe-P-B and  $1.0 \text{ g L}^{-1}$  for  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ , respectively. As can be seen in Fig. 7, the removal rates of OII by  $\text{Fe}_3\text{O}_4$  and Al-Fe-P-B alone are 59.1% and 34.6% after 480 min, respectively. When using  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ , the removal rate can reach 99.3%. It can be observed that  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  is much more efficient than bare  $\text{Fe}_3\text{O}_4$  or Al-Fe-P-B. On the other hand, the calculated apparent pseudo-first-order rate constants of  $\text{Fe}_3\text{O}_4$ , Al-Fe-P-B and  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  are 0.0019, 0.0008 and  $0.0067 \text{ min}^{-1}$  ( $R^2 > 0.99$ ), respectively. The degradation efficiency of OII on  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  is more than the summation of bare  $\text{Fe}_3\text{O}_4$  and Al-Fe-P-B. Thus, there may be a synergistic effect between  $\text{Fe}_3\text{O}_4$  and Al-Fe-P-B. Most authors considered that the synergistic effect resulting by the adsorption property of support caused the difference in the rate of substrate degradation [14,15]. In this study, the adsorption capacity of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  is enhanced dramatically compared with that of bare  $\text{Fe}_3\text{O}_4$ , which corresponds to the specific surface area ( $4.68 \text{ m}^2 \text{ g}^{-1}$  for  $\text{Fe}_3\text{O}_4$  and  $53.02 \text{ m}^2 \text{ g}^{-1}$  for  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ ) of these two catalysts. It means that more dye molecules can be absorbed on the surface of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  than bare  $\text{Fe}_3\text{O}_4$ . The  $\bullet\text{OH}$  generated from the surface reaction between  $\text{H}_2\text{O}_2$  and  $\text{Fe}_3\text{O}_4$  or Al-Fe-P-B may preferentially react with the surface sorbed OII. The enhanced adsorption of OII has a dramatic promotion of its degradation. A similar effect was found by Ramirez et al. [35] that OII adsorption on carbon support had positive effect on degradation. On the other hand, the dispersity of  $\text{Fe}_3\text{O}_4$  nanoparticles was improved after immobilized on Al-Fe-P-B, which can be concluded from the SEM photograph and specific surface area. More active sites of  $\text{Fe}_3\text{O}_4$  nanoparticles are exposed, which results in an increase of the generation of  $\bullet\text{OH}$ . Thus, the OII molecules are effectively decomposed through an adsorption-degradation synergistic process on the surface of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ . The degradation process of OII will be discussed in the next section.

The comparison between  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  and other type of

**Table 1. Degradation efficiency of OII on various catalysts at similar reaction condition (pH=4, reaction time=5 h)**

Catalysts	Degradation efficiency (%)	Reference
Montmorillonite KSF	77.4	[29]
Vanadium-titanium magnetite	30.0	[34]
Carbon-Fe	53.2	[35]
Fe-saponite	51.7	[36]
Zeolite Y-Fe	80.5	[37]
$\text{Fe}_3\text{O}_4/\text{Al-P-B}$	58.7	[21]
$\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$	88.2	Present work

catalyst commonly used in the similar process is listed in Table 1. As can be seen, the performance of  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  is fairly good in comparison to that reported before. Further, there are some distinctive advantages of the novel catalyst over other types, such as low cost, simple synthetic method, environment-friendly and, most important of all, easy to be separated with a magnet. Therefore,  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  could be employed as peroxidase mimetic for removal of OII or other organic pollutant in the present of  $\text{H}_2\text{O}_2$ . With the advantages mentioned above, the novel catalyst may be able to synthesize in a large-scale, which has a huge potential application in the treatment of practical industrial wastewater.

The processes with heterogeneous Fenton catalysts do not only rely on the reactions that occur on the surface of the catalyst, but also on homogeneous reactions in the bulk phase by dissolved iron released from the catalyst [15]. Hence, a special experiment was conducted to investigate the contribution from the homogeneous Fenton reaction. After the heterogeneous degradation experiment, the reaction solution was filtered through a Millipore filter (pore size  $0.22 \mu\text{m}$ ) to remove the solid catalysts. Then  $\text{H}_2\text{O}_2$  and OII were added to the filtrate, to build a homogeneous Fenton reaction system catalyzed by dissolved iron, which is shown in Fig. 7. The removal rate of OII through homogeneous Fenton reaction is below 20% after 480 min. It can be observed that the effect of homogeneous Fenton reaction on the degradation process can be neglected. The whole degradation of OII by  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$  is dominated by heterogeneous Fenton reaction.

## 2-6. The Degradation Process of OII

The OII could be removed efficiently under the optimum reaction conditions. However, it is well accepted that some achromatic medium products, which may have higher toxicity than OII itself, will generate during the degradation process. In the treatment of industrial organic wastewater, the chemical oxygen demand (COD) of the effluent quality is an important indicator. The OII and  $\text{COD}_C$  removal rates during the degradation process have been recorded as shown in Fig. 8. As can be seen, the  $\text{COD}_C$  removal of OII is much slower than its decomposition. Eight hours after the reaction starts the  $\text{COD}_C$  removal rate of OII is about 92.2%. But at the same time the decomposition of OII is nearly 100%. So it could be inferred that some achromatic medium products have not been fully degraded.

To investigate the degradation products, the UV-Vis spectra recorded during the degradation of OII are shown in Fig. 9. The azo-dye is characterized by nitrogen to nitrogen bond ( $-\text{N}=\text{N}-$ ), and the

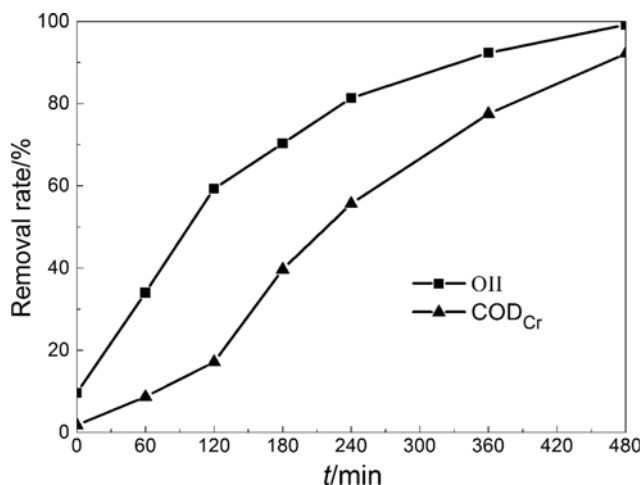


Fig. 8. OII removal rate and COD<sub>Cr</sub> elimination in the OII degradation ( $C_{OII}=0.23 \text{ mmol}\cdot\text{L}^{-1}$ ,  $10 \text{ mmol}\cdot\text{L}^{-1}$  of  $\text{H}_2\text{O}_2$ ,  $1.0 \text{ g}\cdot\text{L}^{-1}$  of catalyst,  $\text{pH}=4$ ,  $40^\circ\text{C}$ ).

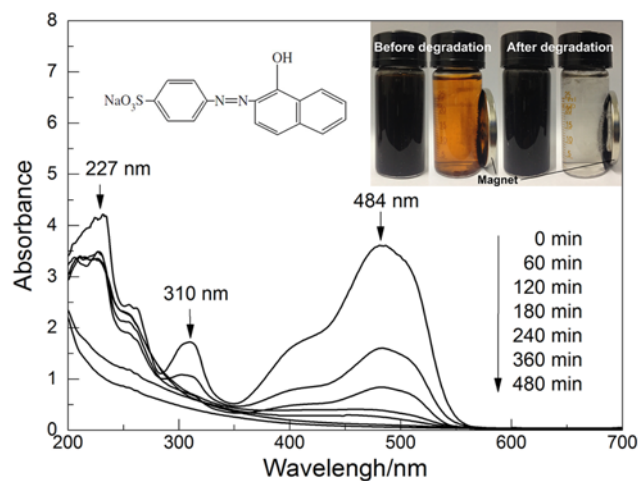


Fig. 9. UV-vis spectra of Orange II as a function of reaction time.

absorption at 484 nm is due to the color of OII solution. The absorption peaks in the ultraviolet region at 227 nm and 310 nm are ascribed to the benzene ring and naphthalene ring, respectively [29]. The results show that the intensity of the 484 nm absorption peak decreases rapidly with the reaction proceeding, indicating that the  $\bullet\text{OH}$  radical first attacks azo groups and destructs the  $-\text{N}=\text{N}-$  bond. And the intensity of the 227 nm and 310 nm absorption peaks gradually decreases, which implies that these two rings are gradually broken. It confirms the fact that  $-\text{N}=\text{N}-$  bond is easier to destruct than aromatic ring structure and also explains why the COD<sub>Cr</sub> removal of OII is much slower than its decomposition. However, these absorption peaks did not completely disappear, related to the uncompleted destruction of some aromatic group, which well corresponds to the COD<sub>Cr</sub> result.

### 3. The Reusability and Stability of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B

The reusability of the catalyst has been evaluated under the reaction conditions which were identical with the first oxidation cycle. After each recycling, the catalyst was treated by magnetic sep-

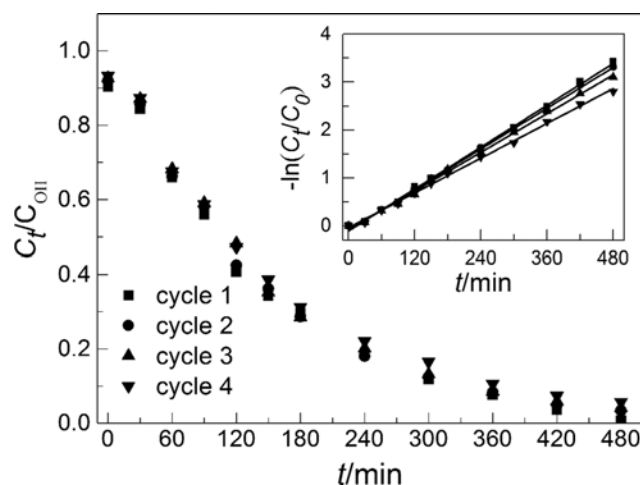


Fig. 10. Effect of recycling the catalyst on the degradation of Orange II ( $C_{OII}=0.23 \text{ mmol}\cdot\text{L}^{-1}$ ,  $10 \text{ mmol}\cdot\text{L}^{-1}$  of  $\text{H}_2\text{O}_2$ ,  $1.0 \text{ g}\cdot\text{L}^{-1}$  of catalyst,  $\text{pH}=4$ ,  $40^\circ\text{C}$ ).

aration, dried and reused. The OII degradation performance on the reused catalyst showed a slight difference with the first oxidation cycle. As shown in Fig. 10, the degradation efficiencies of OII are 99.3%, 96.7%, 95.8% and 94.3% after 480 min for cycle 1, 2, 3 and 4, respectively. All four cycles comply with the pseudo-first-order rate law. It indicates that Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B has a good long-term reusability and activity. The small decrease of catalytic activity is due to the dissolution of iron.

The XRD pattern and Raman spectra of the Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B samples before and after use during the OII degradation are presented in Fig. S6 in supplementary data. It can be seen that there are no obvious change of characteristic peaks before and after oxidation reactions in both XRD pattern and Raman spectra, and the SEM image of the used catalyst is also found to be similar to that of the fresh particles (Fig. 1), which further supports the high stability of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B. The structural stability of Fe<sub>3</sub>O<sub>4</sub> loading on Al-Fe-P-B and the low iron leaking contribute to the stability of the catalytic activity during oxidation reactions. Therefore, the Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B composite is a stable catalyst with long-term reusability and activity.

## CONCLUSION

A novel heterogeneous Fenton catalyst Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B has been successfully prepared by means of in situ growth of spherical-like Fe<sub>3</sub>O<sub>4</sub> nanoparticles on Al-Fe pillared bentonite surface through precipitation oxidization method. The Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B can be used as an efficient heterogeneous catalyst to degrade Orange II in aqueous solution by Fenton-like reaction. The COD<sub>Cr</sub> removal rate of OII is about 92.2% 8 h after the degradation started. The whole degradation process follows pseudo-first-order rate law and mainly occurs on the surface of the catalyst. The enhanced catalytic activity of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B in heterogeneous Fenton system is due to the synergistic effect between Al-Fe-P-B and Fe<sub>3</sub>O<sub>4</sub>. The Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B can achieve solid-liquid separation easily by sample magnetic separation. The novel catalyst has a good reusability and sta-

bility, which will be of potential application in mimicking enzyme catalysis for removal of environmental contaminants.

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### SUPPORTING INFORMATION

Additional information as noted in the text. This information is available via the Internet at <http://www.springer.com/chemistry/journal/11814>.

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## Supporting Information

### Heterogeneous Fenton degradation of Orange II by immobilization of $\text{Fe}_3\text{O}_4$ nanoparticles onto Al-Fe pillared bentonite

Wenbing Li<sup>\*,\*\*,\*†</sup>, Dong Wan<sup>\*,†</sup>, Guanghua Wang<sup>\*,\*\*,\*</sup>, Kun Chen<sup>\*</sup>, Qin Hu<sup>\*</sup>, and Lulu Lu<sup>\*</sup>

<sup>\*</sup>College of Chemical Engineering and Technology, Wuhan University of Science and Technology, Wuhan 430081, China

<sup>\*\*</sup>Hubei Coal Conversion and New Carbon Materials Key Laboratory, Wuhan 430081, China

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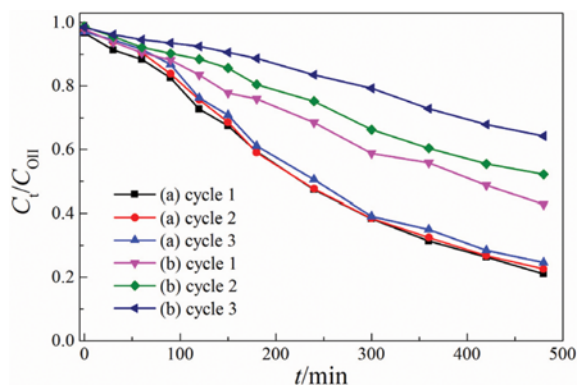


Fig. S1. Effect of recycling the  $\text{Fe}_3\text{O}_4$  nanoparticles on the degradation of Orange II ( $C_{\text{OII}}=0.23 \text{ mmol}\cdot\text{L}^{-1}$ ,  $10 \text{ mmol}\cdot\text{L}^{-1}$  of  $\text{H}_2\text{O}_2$ ,  $1.0 \text{ g}\cdot\text{L}^{-1}$  of  $\text{Fe}_3\text{O}_4$ ,  $\text{pH}=4$ ,  $40^\circ\text{C}$ ).

(a) Precipitation oxidation method, (b) co-precipitation method

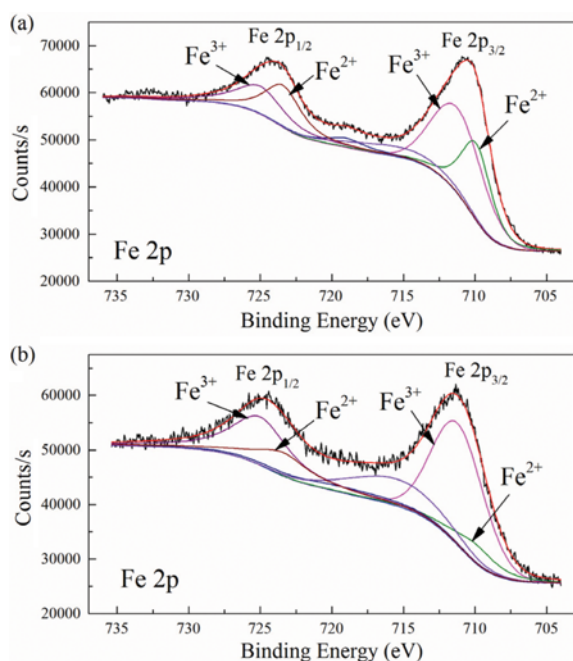


Fig. S2. XPS spectrum of Fe on  $\text{Fe}_3\text{O}_4$  nanoparticles surface synthesized by precipitation oxidation method (a) and co-precipitation method (b) after degradation of OII (Fe 2p line).

The Fe 2p peaks at binding energies (BE) of 711.2 and 725.0 eV with a satellite signal at 719.0 eV are characteristic of  $\text{Fe}^{3+}$ , while the peaks at BE of 709.9 and 723.4 eV with a satellite signal at 715.5 eV are characteristic of  $\text{Fe}^{2+}$ . The components of two oxidation states

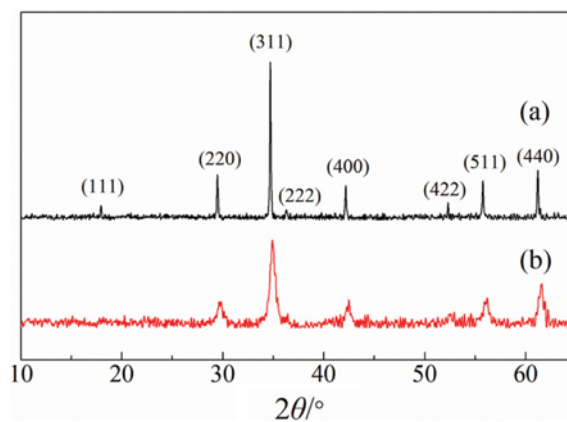


Fig. S3. The XRD patterns of  $\text{Fe}_3\text{O}_4$  nanoparticles synthesized by precipitation oxidation method (a) and co-precipitation method (b).

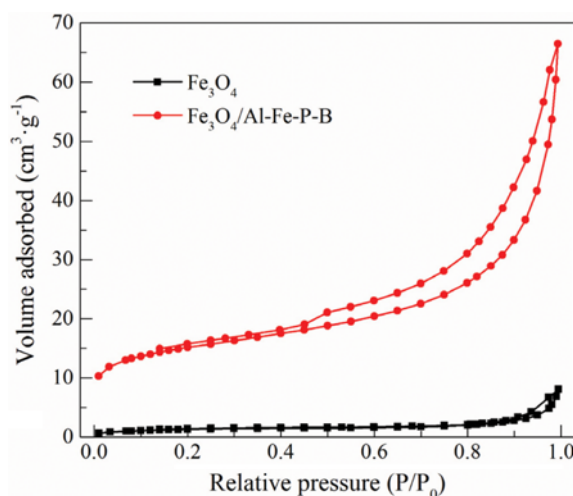


Fig. S4. Nitrogen adsorption/desorption isotherms for  $\text{Fe}_3\text{O}_4$  and  $\text{Fe}_3\text{O}_4/\text{Al-Fe-P-B}$ .

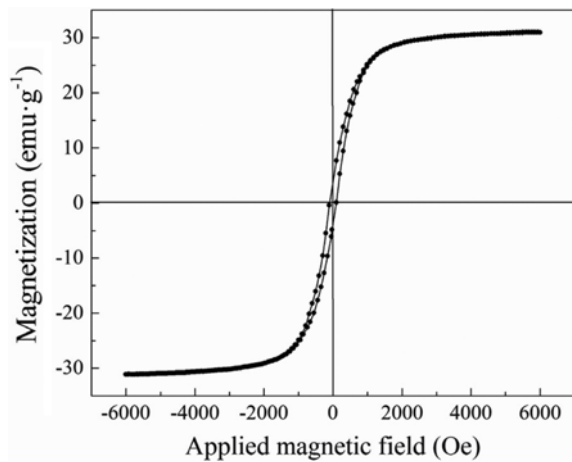


Fig. S5. Hysteresis loop of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B.

of surface iron species are consistent with the binding energy values. In Fig. S1(a), the major component is found to be Fe<sup>3+</sup> which contributes to 69.6% of the total iron surface atoms, while 30.4% of the total iron surface atoms are in the Fe<sup>2+</sup> state. For the sample synthesized by co-precipitation method, the Fe<sup>2+</sup> was found to be 3.8% and Fe<sup>3+</sup> 96.2%, indicating that the outermost surface of Fe<sub>3</sub>O<sub>4</sub> nanoparticles is already oxidized.

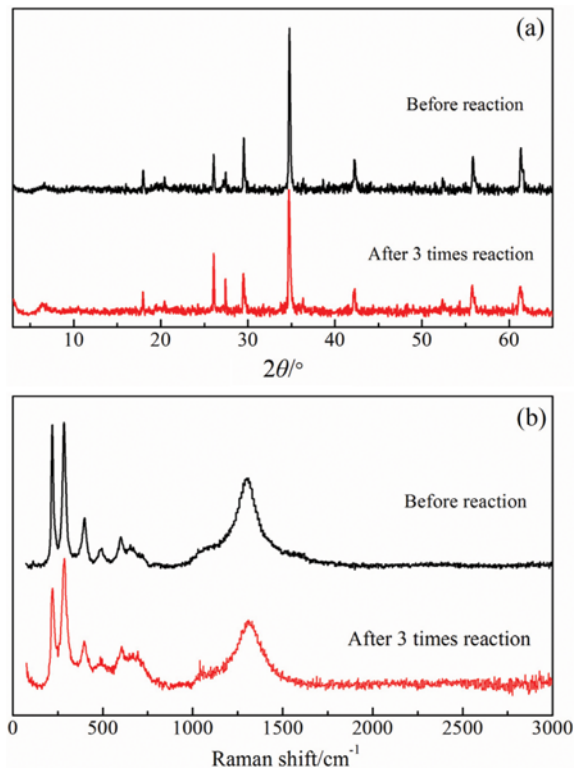


Fig. S6. The XRD pattern (a) and raman spectra (b) of Fe<sub>3</sub>O<sub>4</sub>/Al-Fe-P-B before and after using.