

## Life cycle emissions of greenhouse gas for ammonia scrubbing technology

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**Abstract**—It is thought that the CO<sub>2</sub> emissions from coal-fired power plants contribute greatly to the total anthropogenic CO<sub>2</sub> emissions. Ammonia solvent can be used to absorb the CO<sub>2</sub>, called ammonia scrubbing. However, as has been pointed out, the production of ammonia would emit CO<sub>2</sub>; therefore, the effectiveness of ammonia scrubbing is doubted. The paper focuses on the problem. Two systems are defined in the paper. System I is CO<sub>2</sub> absorption by ammonia scrubbing, and system II is industrial production of ammonium bicarbonate. The total CO<sub>2</sub> emissions of the two systems are calculated by means of life cycle assessment. The paper shows that the total CO<sub>2</sub> emissions of ammonia scrubbing are less than that of the industrial production of fertilizer ammonium bicarbonate. It can be concluded that ammonia scrubbing is an effective way to reduce the anthropogenic CO<sub>2</sub> emissions.

Key words: Ammonia Scrubbing, CO<sub>2</sub> Emissions, Life Cycle Assessment, Coal-fired Power Plant, Ammonia Bicarbonate

### INTRODUCTION

The CO<sub>2</sub> emissions of China are the second largest in the world, to which the combustion of coal contributes about 85%. Some strategies have been produced to control the CO<sub>2</sub> emissions to the atmosphere. These strategies include energy conservation, improvement of energy efficiency, and utilization of renewable energies [1]. However, as the impact of these strategies is limited, it is very important to remove CO<sub>2</sub> from flue gas of coal combustion. Generally, there are six kinds of technologies: chemical solvent absorption, physical adsorption, cryogenic separation, membrane separation, biological fixation as well as the O<sub>2</sub>/CO<sub>2</sub> process. Amongst these techniques, the chemical solvent absorption method is considered as a reliable and relatively low cost method to reduce CO<sub>2</sub> from fossil fuel power plants [2]. Ammonia scrubbing is one of chemical solvent absorption methods, which is widely used in the fertilizer industry, is proven experimentally to be more effective than MEA scrubbing that is so far the most acceptable method [3]. However, the production of ammonia will produce CO<sub>2</sub> also. So the effectiveness of ammonia scrubbing has been doubted. The paper focuses on the problem. The following part will give an introduction of ammonia scrubbing technology. Then two systems are defined: one is the ammonia scrubbing system; the other is the industry production of the fertilizer ammonium bicarbonate. Based on the systems, life cycle CO<sub>2</sub> emissions are evaluated.

### AMMONIA SCRUBBING TECHNOLOGY

Ammonia scrubbing technology involves spraying aqueous ammonia into the flue gas of a power plant to capture CO<sub>2</sub>. The NH<sub>3</sub> will react with CO<sub>2</sub> to produce ammonium bicarbonate [4,5]. The

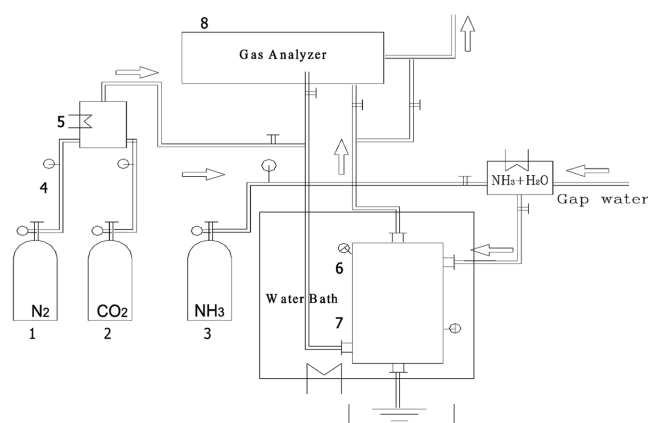


Fig. 1. Experimental setup of ammonia scrubbing.

- |                             |                           |
|-----------------------------|---------------------------|
| 1. N <sub>2</sub> Cylinder  | 5. Electronic heater      |
| 2. CO <sub>2</sub> Cylinder | 6. Temperature controller |
| 3. NH <sub>3</sub> Cylinder | 7. Reaction column        |
| 4. Mass flow controller     | 8. Gas analyzer           |

gas-liquid chemical reactions can be expressed by the following reaction equation:



Experimental study on ammonia scrubbing was done at the Department of Thermal Engineering, Tsinghua University. The experimental setup is shown in Fig. 1. The reactor, which was made of stainless steel with inside diameter of 250 mm and height of 450 mm, was installed in a temperature controlled water bath. The main part of the experimental system is composed of a sieve-plate tower, which is gas-stream reverse flow. Its schematic diagram is shown in Fig. 2. Five layers of sieve plates, which were made of stainless steel with thickness of 3 mm and bore diameter of 3 mm, are set in the reactor in order to make CO<sub>2</sub> and the NH<sub>3</sub> solution react thoroughly.

Studies on CO<sub>2</sub> removal by ammonia scrubbing have been per-

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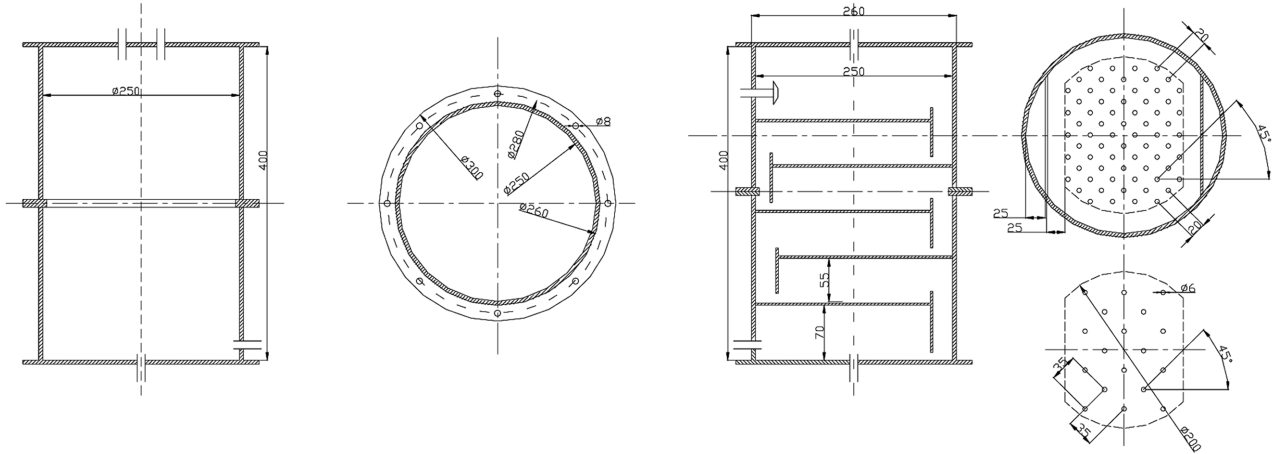


Fig. 2. The structure and parameters of the absorption tower.

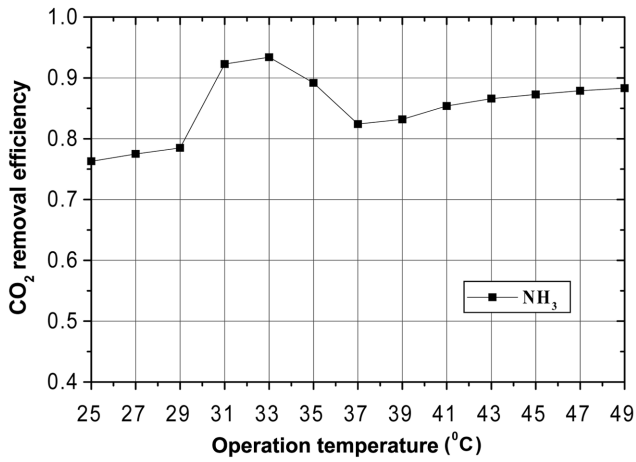


Fig. 3. CO<sub>2</sub> removal efficiency as a function of operation temperature. The operating conditions were at CO<sub>2</sub> inlet concentration of 12% (v/v), and ammonia concentration of 0.066 mol/l.

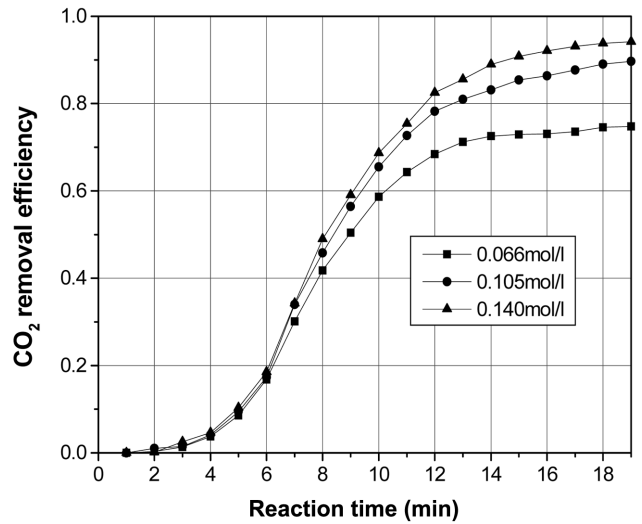


Fig. 5. CO<sub>2</sub> removal efficiency as a function of reaction time for various ammonia solution concentrations. The operating conditions were at CO<sub>2</sub> inlet concentration of 12% (v/v), water bath temperature of 28 °C.

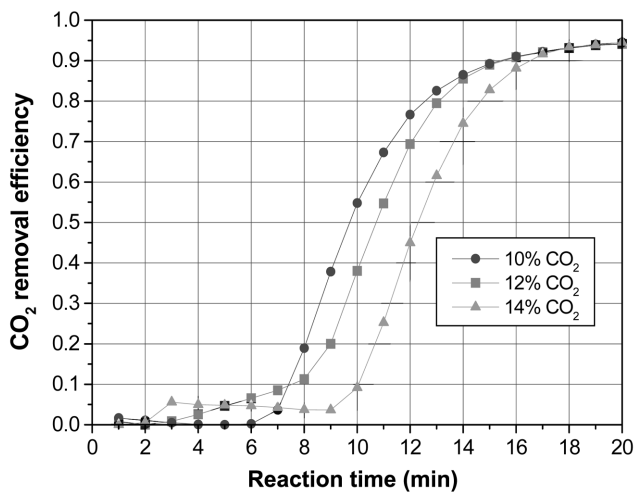


Fig. 4. CO<sub>2</sub> removal efficiency as a function of reaction time for various CO<sub>2</sub> concentrations. The operating conditions were at water bath temperature of 28 °C, and ammonia concentration of 0.140 mol/l.

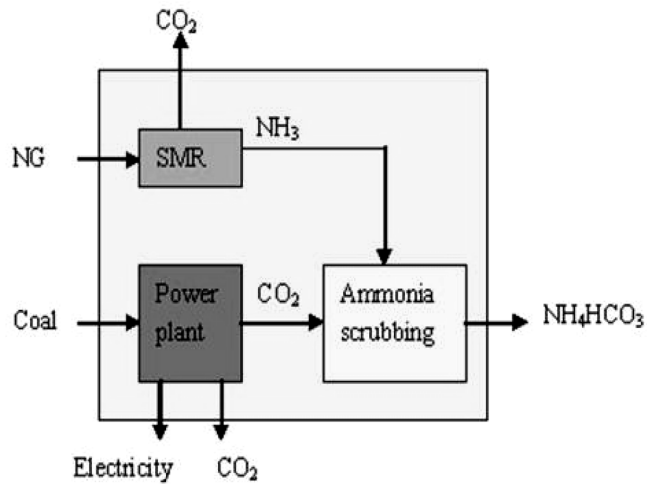


Fig. 6. Schematic of system I.

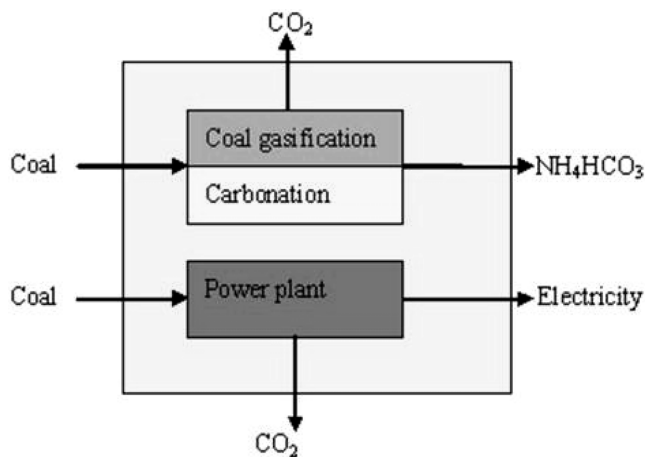


Fig. 7. Schematic of system II.

formed in an open continuous flow reactor. The temperature of the ammonia solution was designed to be in the range from 25 to 55 °C. The inlet concentrations of CO<sub>2</sub> were 10%, 12% and 14% (v/v), and the ammonia solution concentrations were 0.066, 0.105 and 0.140 mol/l, respectively. Some results can be seen in Figs. 3, 4, and 5. The overall CO<sub>2</sub> removal efficiencies in this study can be above 95% when the reaction temperature is about 33 °C. It is proved that ammonium bicarbonate is the main product of the CO<sub>2</sub>-NH<sub>3</sub> reaction in this study.

Although ammonium bicarbonate is a cheap and widely used fertilizer in China, it is easily decomposed. Lately, some researchers have made great progress in the area of long effect ammonium bicarbonate, so ammonium bicarbonate is promising to be a fine fertilizer. If the need for large amounts of ammonia is not satisfied, the crystalline products can be heated to release CO<sub>2</sub> and NH<sub>3</sub>, as shown in Eq. (2).



CO<sub>2</sub> and NH<sub>3</sub> can be segregated to have sequestration ready CO<sub>2</sub>, and the ammonia solution is thus recycled and used as the scrubbing agent.

#### SYSTEM BOUNDARY SETTING

Two systems are defined in order to compare the life cycle CO<sub>2</sub> emissions. System I is CO<sub>2</sub> absorption by ammonia scrubbing, which includes three parts: ammonia production by steam methane reform (SMR), coal-fired power plant with installed capacity 300 MW, and CO<sub>2</sub> absorption by ammonia scrubbing with the byproduct ammonium bicarbonate. System II is industry production of ammonium bicarbonate, which includes three parts: syngas production by coal gasification, ammonium bicarbonate production by carbonation, and coal-fired power plant with installed capacity 300 MW.

One point needing to be explained is the reason that coal is used to produce ammonium bicarbonate through gasification and carbonation, not natural gas. Coal gasification can produce enough CO<sub>2</sub> that is used to produce ammonium bicarbonate. However, CO<sub>2</sub> must be produced in some other way if SMR is used because SMR cannot afford enough CO<sub>2</sub> for production of ammonium bicarbonate. For simplification, coal gasification is used in system II.

The function unit is the yearly yield of ammonium bicarbonate with ammonia scrubbing to absorb the yearly CO<sub>2</sub> emissions of 300 MW coal-fired power plant, as well as the yearly electricity generated by the power plant.

#### LIFE CYCLE CO<sub>2</sub> EMISSIONS

##### 1. General Information for Calculation

The coal-fired power plant is assumed to operate at rate capacity for 7,000 hours per year. Therefore the total electricity generated is about  $2.1 \times 10^9$  kWh per year. In China, the CO<sub>2</sub> emission factor for coal-fired power plant is about 0.8 kg/kWh. Then the annual CO<sub>2</sub> emissions are about  $1.68 \times 10^6$  tonnes. The CO<sub>2</sub> removal efficiency of ammonia scrubbing is about 95%. It is assumed that the product is fully ammonium bicarbonate. Then the annual ammonium bicarbonate can be as large as  $2.87 \times 10^6$  tonnes.

Therefore, the unit function can be described as electricity of  $2.1 \times 10^9$  kWh and ammonium bicarbonate of  $2.87 \times 10^6$  tonnes.

##### 2. CO<sub>2</sub> Emissions of System I

At present, the absorption ability of ammonia is about 0.85-1.2 kgCO<sub>2</sub>/kgNH<sub>3</sub> [3]. The excess ammonia can be recycled to absorb CO<sub>2</sub> again. Then the total absorption factor is about 2.5 kgCO<sub>2</sub>/kg NH<sub>3</sub>. The annual ammonia consumption will be  $0.64 \times 10^6$  tonnes.

For industry production of ammonia by SMR, the CO<sub>2</sub> emission factor is about 1.22 t CO<sub>2</sub> per tonne ammonia [6] (It is 0.97 in theory). Therefore, the annual CO<sub>2</sub> emissions by SMR are about  $0.78 \times 10^6$  tonnes.

For the ammonia scrubbing process, about 130 kWh electricity is used per tonne ammonium bicarbonate [7]. To produce the electricity, additional CO<sub>2</sub> will be emitted, about 104 kgCO<sub>2</sub>/tonne. For the annual production of ammonium bicarbonate, the CO<sub>2</sub> emissions will be  $0.3 \times 10^6$  tonnes.

Not considering the CO<sub>2</sub> emissions in the other process such as transportation, the total CO<sub>2</sub> emissions of system I can be evaluated as 1.16 Mt.

##### 3. CO<sub>2</sub> Emissions of System II

For industrial production of ammonium bicarbonate by coal gasification, the material consumption is 0.25 tonnes of NH<sub>3</sub>, and 0.65 tonnes of CO<sub>2</sub> for one tonne of NH<sub>4</sub>HCO<sub>3</sub> [7]. For coal gasification, the CO<sub>2</sub> emission factor is about 3.59 tonnes per tonne NH<sub>3</sub> [6]. It can be seen that there is excess CO<sub>2</sub> for NH<sub>4</sub>HCO<sub>3</sub> production in the coal gasification process, which is about 0.248 tonnes per tonne NH<sub>4</sub>HCO<sub>3</sub>. Same as in system I, the additional CO<sub>2</sub> emission will be 104 kg CO<sub>2</sub>/tonne NH<sub>4</sub>HCO<sub>3</sub> for electricity consumption. Therefore the annual CO<sub>2</sub> emissions in the process are about 1.01 Mt. Putting the CO<sub>2</sub> emissions of power plant together, the total CO<sub>2</sub> emissions of system II can be evaluated as 2.69 Mt.

All the calculations above are summarized in Table 1.

##### 4. Discussions

Due to the lack of data information, the consumption of water, steam, and catalysis in both systems is not involved in the analysis. Their production will emit CO<sub>2</sub> also from the point of view of life cycle. The CO<sub>2</sub> emissions during the manufacturing of equipment are overlooked also. According to experience of life cycle assessment [8], the CO<sub>2</sub> emissions from these overlooked factors are generally less than 5% of total emissions of the system. Therefore, the simplification will not affect the results.

**Table 1. Summary of the calculation**

No.	Item	Unit	Equation	Result
(1)	Electricity Production	kWh	$7,000 \times 300 \times 10^3$	$2.1 \times 10^9$
(2)	CO <sub>2</sub> emissions of PP	tonne	$(1) \times 0.8 \times 10^{-3}$	$1.68 \times 10^6$
(3)	NH <sub>4</sub> HCO <sub>3</sub> production	tonne	$(2) \times 0.95 \times 79/44$	$2.87 \times 10^6$
(4)	Ammonia production	tonne	$(2) \times 0.95/2.5$	$0.64 \times 10^6$
(5)	CO <sub>2</sub> emissions of SMR	tonne	$(4) \times 1.22$	$0.78 \times 10^6$
(6)	CO <sub>2</sub> emissions for electricity consumption in the process of NH <sub>4</sub> HCO <sub>3</sub> production	tonne	$0.8 \times 10^{-3} \times 130 \times (3)$	$0.3 \times 10^6$
(7)	CO <sub>2</sub> emission factor of CG	tonne/tonne	$3.59 \times 0.25 - 0.65$	0.248
(8)	CO <sub>2</sub> emissions of CG	tonne	$(7) \times (3)$	$0.71 \times 10^6$
(9)	CO <sub>2</sub> emissions of system I	tonne	$(2) \times 0.05 + (5) + (6)$	$1.16 \times 10^6$
(10)	CO <sub>2</sub> emissions of system II	tonne	$(2) + (6) + (8)$	$2.69 \times 10^6$

1. PP is simplification for Power Plant.

2. CG is simplification for Coal Generation.

## CONCLUSIONS AND SUGGESTIONS

From the analysis of the paper, it can be concluded that the life cycle CO<sub>2</sub> emissions of ammonia scrubbing are about 1.16 Mt a year for a 300 MW coal-fired power plant, whereas 2.69 Mt for industry production process of ammonium bicarbonate. It can be concluded that ammonia scrubbing is an effective way to absorb CO<sub>2</sub> from the flue gas of coal-fired power plants.

The difference in life cycle CO<sub>2</sub> emissions between the two systems is due to the ammonia originating from different sources. Less CO<sub>2</sub> emission of system I is due to the ammonia originating from natural gas, instead of coal in system II. Therefore, ammonia originating from low-carbon sources is significant from the point of view of CO<sub>2</sub> removal.

Furthermore, decomposing ammonium bicarbonate to regenerate ammonia is a better option rather than using it as a kind of fertilizer.

## ACKNOWLEDGMENT

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